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## Low temperature synthesis of ion sieve for lithium recovery from brines

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## PURPOSE OF THE ABSTRACT

Mainly used in Li-Ion batteries (65% of the market), lithium is a coveted raw material, more available in brines in dissolved form than in the continental crust. Generally, lithium in brine is recovered by a simple evaporation process over several months. An alternative method, using ion sieves, has been tested with the objective of faster lithium recovery (1).

The ion sieve, with its high ionic selectivity and its important regenerative power, is a key material for the exploitation of lithium brines. The  $\text{Li}_2\text{TiO}_3$  (LTO) phase is particularly investigated due to its high  $\text{Li}/\text{Ti}=2$  ratio and reversible  $\text{Li}^+-\text{H}^+$  exchange allowing  $\text{Li}^+$  capture and release (2). In addition, this material offers real industrial interest considering its chemical stability and low production cost.

Among processes to produce LTO particles, hydrothermal synthesis, allowing a possible morphological modification of particles and size tuning at the nanoscale, is for choice as compared to the solid-state method (3,4).

The hydrothermal synthesis is usually composed of two steps. The first one is the formation of a metastable cubic  $\alpha\text{-Li}_2\text{TiO}_3$  (space group  $\text{Fm-3m}$ ), starting from anatase particles dispersed in concentrated lithium hydroxide solution in autoclave with temperatures ranging from  $120^\circ\text{C}$  to  $200^\circ\text{C}$ . The resulting powder is then heated at high temperature (ranging from  $300^\circ\text{C}$  to  $700^\circ\text{C}$ ) to obtain a monoclinic  $\beta\text{-Li}_2\text{TiO}_3$  (space group  $\text{C}/2\text{c}$ ) recognizable in XRD, and considered as the relevant crystallographic phase for  $\text{Li}^+$  exchange according to literature. Literature shows that hydrothermally synthesized particles are performant for Li recovery, nevertheless hydrothermal processes are expensive to implement at an industrial scale due to the considered pressure. As a consequence, the first step must be reconsidered.

The aim of this study was to synthesize LTO using softer conditions and especially under atmospheric pressure, which is the key to an industrially acceptable process. This material must have better or equal capture performance as the products resulting from hydrothermal syntheses listed in the literature.

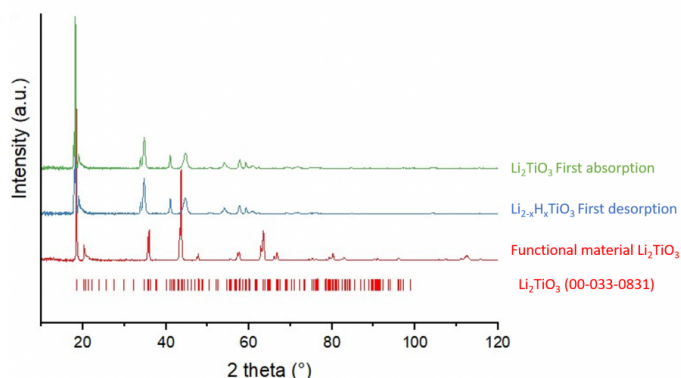
In our study, instead of using autoclave under autogenous pressure, the synthesis was performed at lower temperatures (approximately  $100^\circ\text{C}$ ) than usual to allow the use of atmospheric pressure reactors. Energy and chemical costs were minimized by changing the titanium precursor (homemade precipitate vs commercial titania), reducing the ratio  $\text{Li}/\text{Ti}$  necessary to get the right phase, lowering the synthesis time and the temperature under the reflux temperature. After a heating of the resulting powders at  $700^\circ\text{C}$ , the products from this parametric study were characterized in XRD, SEM, TEM and BET to characterize the structural and textural changes.

Once the ion sieve has been synthesized after these two steps, the lithium has to be removed by  $\text{H}^+$  ion-exchange to get an activated product able to capture  $\text{Li}^+$ . This ion-exchange takes place upon treatment with a certain concentration of chlorhydric acid to form  $\text{Li}_2\text{-xHxTiO}_3$ , with  $x$  depending on desorption rate of the

material with  $\text{Li}_2\text{TiO}_3$  and  $\text{H}_2\text{TiO}_3$  as end-members. This activated titanate  $\text{Li}_{2-x}\text{H}_x\text{TiO}_3$  can reversibly exchange  $\text{H}^+$  by  $\text{Li}^+$  from brine.

The best product resulting from this new synthesis exhibited the same capture performance as the materials reported in the literature. The concentration of desorbed and absorbed lithium was monitored by atomic absorption spectroscopy and the synthesized material had a lithium exchange capacity of  $33 \text{ mg}\cdot\text{g}^{-1}$  (mg of Li per g of material), which represents 26% of the maximum (theoretical) lithium exchange capacity. By continuously monitoring the exchanges, kinetics could be described in order to find the optimal cycle time to maximize the average quantity of lithium recovered per time unit. Based on all these results, a scale-up synthesis (34L) could be initiated, which paves the way to a continuous industrial process for lithium recovery from brines.

## FIGURES



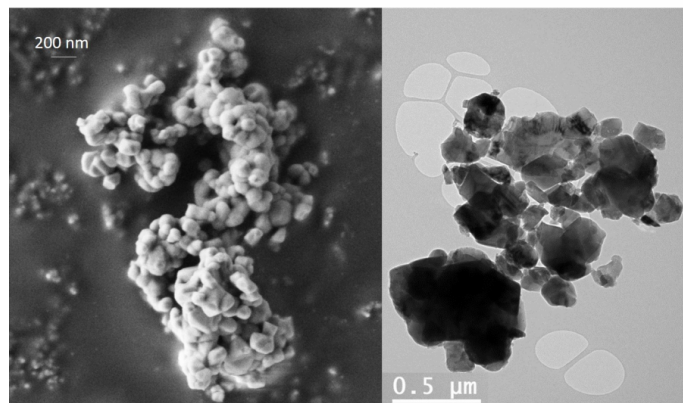
**FIGURE 1**

XRD product after synthesis, first desorption and first absorption

In red the functional material after synthesis and its indexation (00-033-0831) (reference 5)

In blue, the functional material Li(2-x)TiO<sub>3</sub> after the first desorption.

In green, the functional material Li<sub>2</sub>TiO<sub>3</sub> after the first absorption



**FIGURE 2**

Scanning and transmission electron micrograph of the functional material Li<sub>2</sub>TiO<sub>3</sub>

Left to the picture: Scanning electron micrograph of the functional material Li<sub>2</sub>TiO<sub>3</sub>

Right to the picture: Transmission electron micrograph of the functional material Li<sub>2</sub>TiO<sub>3</sub>

## KEYWORDS

Water lithium resources | Lithium ion-sieve technology | Lithium adsorption/desorption mechanisms | Lithium titanate oxide

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